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APPLICATION FOR

UNITED STATES LETTERS PATENT

FOR

RESONANT ACOUSTIC TRANSMITTER APPARATUS AND METHOD FOR SIGNAL TRANSMISSION

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BACKGROUND OF THE INVENTION

1. Related Applications

This application is a continuation-in-part of United States Patent Application Ser. No. 09/676,906 filed on October 2, 2000 now pending and which is hereby incorporated in its entirety herein by reference.

2. Field of the Invention

This invention relates generally to oil field tools, and more particularly to acoustic data telemetry devices for transmitting data from a downhole location to the surface.

3. Description of the Related Art

To obtain hydrocarbons such as oil and gas, boreholes are drilled by rotating a drill bit attached at a drill string end. A large proportion of the current drilling activity involves directional drilling, i.e., drilling deviated and horizontal boreholes, to increase the hydrocarbon production and/or to withdraw additional hydrocarbons from the earth's formations. Modern

directional drilling systems generally employ a drill string having a bottomhole assembly (BHA) and a drill bit at end thereof that is rotated by a drill motor (mud motor) and/or the drill string. A number of downhole devices in the BHA measure certain downhole operating parameters associated with the drill string and the wellbore. Such devices typically include sensors for measuring downhole temperature, pressure, tool azimuth, tool inclination, drill bit rotation, weight on bit, drilling fluid flow rate, etc. Additional downhole instruments, known as measurement-while-drilling ("MWD") and logging-while-drilling ("LWD") devices in the BHA provide measurements to determine the formation properties and formation fluid conditions during the drilling operations. The MWD or LWD devices usually include resistivity, acoustic and nuclear devices for providing information about the formation surrounding the borehole.

The trend in the oil and gas industry is to use a greater number of sensors and more complex devices, which generate large amounts of measurements and thus the corresponding data. Due to the copious amounts of downhole measurements, the data is typically processed downhole to a great extent. Some of the processed data must be telemetered to the surface for the operator and/or a surface control unit or processor device to control the drilling operations, which may include

altering drilling direction and/or drilling parameters such as weight on bit, drilling fluid pump rate, and drill bit rotational speed. Mud-pulse telemetry is most commonly used for transmitting downhole data to the surface during drilling of the borehole. However, such systems are capable of transmitting only a few (1-4) bits of information per second. Due to such a low transmission rate, the trend in the industry has been to attempt to process greater amounts of data downhole and transmit only selected computed results or "answers" uphole for controlling the drilling operations. Still, the data required to be transmitted far exceeds the current mud-pulse and other telemetry systems.

Although the quality and type of the information transmitted uphole has greatly improved since the use of microprocessors downhole, the current systems do not provide telemetry systems, which are accurate and dependable at low frequencies of around 100 Hz.

Acoustic telemetry systems have been proposed for higher data transmission rates. Piezoelectric materials such as ceramics began the trend. Ceramics, however require excessive power and are not very reliable in a harsh downhole environment. Magnetostrictive material is a more suitable material for downhole application. Magnetostrictive material

is a material that changes shape (physical form) in the presence of a magnetic field and returns to its original shape when the magnetic field is removed. This property is known as magnetostriction.

Certain downhole telemetry devices utilizing a magnetostrictive material are described in U.S. Patent 5,568,448 to Tanigushi et al. and 5,675,325 to Taniguchi et al. These patents disclose the use of a magnetostrictive actuator mounted at an intermediate position in a drill pipe, wherein the drill pipe acts as a resonance tube body. An excitation current applied at a predetermined frequency to coils surrounding the magnetostrictive material of the actuator causes the drill pipe to deform. The deformation creates an acoustic or ultrasonic wave that propagates through the drill pipe. The propagating wave signals are received by a receiver disposed uphole of the actuator and processed at the surface.

The above noted patents disclose that transmission efficiency of the generated acoustic waves is best at high frequencies (generally above 400hz). The wave transmission, however drops to below acceptable levels at low frequencies (generally below 400 hz). An acoustic telemetry system according to the above noted patents requires precise placement of the actuator and unique "tuning" of the drill pipe section with the

magnetostrictive device in order to achieve the most efficient transmission, even at high frequencies.

The precise placement requirements and low efficiency is due to the fact that such systems deform the drill pipe in order to induce the acoustic wave. In such systems, the magnetostrictive material works against the stiffness of the drill pipe in order to deform the pipe. Another drawback is that the deformation tends to be impeded by forces perpendicular ("normal" or "orthogonal") to the longitudinal drill pipe axis. In downhole applications, extreme forces perpendicular to the longitudinal drill pipe axis are created by the pressure of the drilling fluid ("mud") flowing through the inside of the drill pipe and by formation fluid pressure exerted on the outside of the drill pipe. Although the pressure differential across the drill pipe surface (wall) approaches zero with proper fluid pressure control , compressive force on the drill pipe wall remains. Deformation of the drill pipe in a direction perpendicular to the longitudinal axis is impeded, because the compressive force caused by the fluid pressure increases the stiffness of the drill pipe.

The present invention addresses the drawbacks identified above by using an acoustic actuator source to resonate a reaction mass separated from the portion of the tube body through which acoustic wave

transmission occurs. With a large reaction mass, efficient transmission can be achieved even at relatively low frequencies (below 400 Hz).

SUMMARY OF THE INVENTION

To address some of the deficiencies noted above, the present invention provides an apparatus and a method for transmitting a signal from a downhole location through the drill or production pipe at low frequencies with high efficiencies. The present invention also provides a MWD, completion well and production well telemetry system utilizing an actuator and reaction mass to induce an acoustic wave indicative of a parameter of interest into a drill pipe or production pipe.

The present invention includes a well system having a sensor for detecting at least one parameter of interest downhole; a controller for converting an output of the sensor to a first signal indicative of the at least one parameter of interest; at least one signal conducting mass; at least one actuator in communication with the at least one signal conducting mass for receiving the first signal from the controller and for inducing an acoustic wave representative of the first signal into the signal conducting mass; a reaction mass in communication with the at least one actuator wherein the

signal conducting mass is coupled to the reaction mass by the at least one actuator; an acoustic wave receiver disposed in the at least one signal conducting mass for receiving the acoustic wave and for converting the acoustic wave to a second signal indicative of the at least one parameter of interest; and a processor for processing the second signal from the acoustic wave receiver and for delivering the processed second signal to an output device.

BRIEF DESCRIPTION OF THE DRAWINGS

For detailed understanding of the present invention, references should be made to the following detailed description of the preferred embodiment, taken in conjunction with the accompanying drawings, in which like elements have been given like numerals and wherein:

Figures 1A and 1B show schematic drawings of the conceptual difference between the present invention and prior art identified herein.

Figure 2 is a cross section schematic showing a free reaction mass embodiment of the present invention.

Figure 3 is a cross section schematic showing a reaction mass embodiment of the present invention.

Figure 4A is a schematic showing an embodiment of the present invention wherein the reaction mass is created by a "dead end" wherein the entire pipe moves axially with respect to force application members.

Figure 4B is a detailed schematic of a magnetostrictive device mounted with force application members on a sleeve coupled to a drill pipe, which allows axial movement of the entire pipe relative to the sleeve.

Figure 4C is a schematic showing an embodiment of the present invention wherein the reaction mass is created by a "dead end" wherein only an upper section of pipe moves axially with respect to force application members.

Figure 4D is a detailed schematic of a magnetostrictive device mounted between a lower section of pipe and an upper section of pipe such that only the upper section of pipe moves axially with respect to force application members mounted on the lower section of pipe.

Figure 5 is an elevation view of a drilling system in a MWD arrangement according to the present invention.

Figure 6 is an elevation view of a production well system according to the present invention.

Figure 7 is a conceptual schematic diagram of an alternative embodiment of the present invention.

Figures 8A-8B show two embodiments of the present invention having different fluid flow paths with respect to a reaction mass.

Figure 9A is an alternative embodiment of the present invention wherein a valve is used to restrict flow of pressurized drilling fluid to excite an acoustic actuator.

Figure 9B is an alternative embodiment wherein the reaction mass is a hollow tube and a valve is used to restrict fluid flow to initiate oscillation of the hollow tube.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Figure 1A is a schematic diagram of a system **100a** illustrating the concept of the present invention while **Figure 1B** shows the concept of a prior art telemetry systems **100b** described above. In each case, an acoustic wave travels through a drill pipe or other tube-like mass **101a** and **101b** respectively, which acoustic wave is received by a corresponding receiver **104a** and **104b**. In the present invention, the acoustic wave is generated by an actuator, which is described below in more detail with respect to specific embodiments. In the configuration of **Figure 1B,** the acoustic wave is generated by applying a force **102b** against surfaces **108** and **109** within a cavity formed in the wall of the drill pipe **101b**. The force **102b** works against the stiffness of the drill pipe **101b**. The stiffness of the pipe acts as a damping force, which requires a large amount of power to induce a sufficient portion of the force **102b** axially into the drill pipe **101b** to generate the acoustic wave. Such a system is relatively inefficient. In addition, it has been found that a system such as system **100b** is even less effective at frequencies below 400 Hz compared to frequencies above 1000 Hz. Furthermore, systems such as **100b** require exact placement of and unique "tuning" of the drill pipe section containing the magnetostrictive actuator. The United States Patents 5,568,448 and 5,675,325 noted

above indicate that the optimum placement of the actuator in a drillpipe section is substantially midway between an upper and a lower end of the drill pipe section.

In the system **100a** of the present invention a force **102a** reacts with a reaction mass **106** and the drill pipe **101a** in a manner that eliminates or substantially reduces the damping effects of the drill pipe stiffness. The mass of the reaction mass **106** is selected to be much greater than the mass of the drill pipe **101a** so that the force **102a** can "lift" or move the drill pipe **101a** away from the reaction mass **106** with relatively negligible displacement of the reaction mass **106**. The overall resultant force **102a** is transferred to the drill pipe **101a**. In this manner, a much greater portion of the force generated by the actuator is transmitted to the drill pipe **101a** in the system configuration of **Figure 1A** compared to the configuration shown in **Figure 1B**. In an alternative embodiment, the mass of the reaction mass may be reduced when the actuator is used to oscillate the reaction mass at a high amplitude with a relatively low frequency. The system of **Figure 1A** requires substantially less power to induce an acoustic wave into the drill pipe compared to the system of **Figure 1B**. The acoustic wave induced in the drill pipe **101a** is detected by an acoustic receiver **104a** located near the surface.

Figure 2 is a cross section schematic diagram of an acoustic telemetry system **200** according to one embodiment of the present invention. This telemetry system **200** includes a reaction mass **204**, which may be a lower section **201** of a drill string **200** and a substantially free section **202**, which may be an upper section **202** of the drill string **200**. The free section **202** is preferably a drill pipe. An acoustic actuator **206** including a force application member **207** made from a suitable magnetostrictive material, such as Terfenol-D® is disposed around a portion **209** of the reaction mass **204**. When current is applied to coils (not shown) surrounding the force application member **207**, a magnetic field is created around the member **207.** This magnetic field causes the magnetostrictive material **207** to expand along the longitudinal axis **203** of the drill pipe **202**. Removing the current from the coils causes the magnetostrictive material **207** to contract to its original or near-original position. Repeated application and removal of the current to the coils at a selected frequency causes the actuator **206** to apply force on the section **202** at the selected frequency. This action induces an acoustic wave in the drill pipe **202.** The acoustic wave is detected by a dector or receiver (described later) that is placed spaced apart from the actuator **206**.

The drill string includes one or more downhole sensors (not shown) which provide to a controller signals representative of one or more for parameters of interest, which may include a borehole parameter, a parameter relating to the drill string and the formation surrounding the wellbore. The controller converts the sensor signal to a current pulse string, and delivers the current pulse string to the coils of actuator **206**. With each current pulse, the actuator expands, thereby applying a force to the transmission mass 28. of the drill string **200** and to the reaction mass **204**.

The upper section **202** is in a movable relationship with the lower section **201** such that the lower section **201** applies a compressive force to the magnetostrictive material **207**. The actuator **206** is restrained at a lower end **212** by a restraining lip or portion **214** of the upper section **202**. A compression spring **210** ensures that a selected amount of compression remains on the force application member **207** at all times. Stops or travel restrictors **208** provide control of the relative movement between the lower section **201** and the actuator **206**.

In the embodiment of **Figure 2**, the drill string **200** is assembled such that the effective mass of the lower section **201** is much greater than

the mass of the upper section **202**. When current is applied to the coils of the actuator **206**, magnetostriction in the actuator creates an acoustic wave in the upper section **202**. Since the effective mass of the lower section **201** is much greater than that of the upper section **202**, most of the acoustic wave travels in the upper section **202**. The pressure exerted on the inner wall **216** of the drill string **200** by drilling mud **219** flowing therethrough has little negative effect on the efficiency of the present invention, because the device of **Figure 2** does not rely on flexing the drill string section **204** or **202** in a direction perpendicular to the longitudinal axis **203** of the drill string **200**.

Figure 3 is a cross section schematic showing an alternative reaction mass embodiment for the acoustic telemetry system of the present invention. In this embodiment, a reaction mass **306** with its associated weight **w** is suspended within a drill string section **300** that includes a drill pipe **302**. A substantial portion of the weight of the reaction mass **306** is born by a magnetostrictive actuator **304** at an upper end **314** of the actuator. The actuator **304** is restrained from downward axial movement downward by a restraining lip or portion **316** and upward axial movement being restrained by the reaction mass **306**. A rotational restraining device such as pins **310** may be used to minimize energy losses from non-axial

movement and to ensure that forces generated by the actuator **304** are directed into the drill pipe **302**.

The actuator **304** includes a force application member **207** similar to the member shown in **Figure 2**. For effective transfer of actuator energy to the drill pipe **302**, the force application member **207** is maintained under a certain amount of compression at all times. To provide the compression, a spring **308** may be disposed above the reaction mass **306**. A retention device **312** provides an upper restraint for the spring **308**. The retention device **312** is attached to the drill pipe **302** in a fixed manner to inhibit or prevent movement of the retention device **312** relative to the drill pipe **302**. With this arrangement, the drill pipe **302** is longitudinally displaced by forces generated by the magnetostrictive actuator **304**.

The operation of the embodiment shown in **Figure 3** is similar to the operation of the embodiment shown in **Figure 2**. The main distinction is that the reaction mass in **Figure 2** is the lower section **204** of the drill string **200**, while the reaction mass **306** in **Figure 3** is not an integral part of the drill string section **300**.

The embodiment of **Figure 3** uses one or more downhole sensors (not shown) associated with the drill string to provide signals representing one or more parameters to a controller (not shown). The controller converts the sensor signals to a current pulse string and delivers the string of pulses to the coils of actuator **304** at a selected frequency. With each current pulse, the actuator **304** as applies a force to the drill pipe **302** and to the reaction mass **306**. The weight of the reaction mass **306** is selected to be sufficiently larger so that a the drill pipe **302** is moved axially away from the reaction mass **306** and returned to the original position at the selected frequency, thereby creating an acoustic wave in the drill pipe **302**. The acoustic wave is then received by a receiver (not shown) that is positioned spaced apart from the actuator **304** .

Figure 4A is a schematic showing an embodiment of a portion of a telemetry system **400** according to the present invention wherein the reaction mass is created by a "dead end" **406** . This embodiment can be especially useful in completion and production well applications. In the embodiment of **Figure 4A**, an anchor mechanism or device **406** which may be expandable pads or ribs, is disposed on the pipe **410.** The device **406** can be selectively operated to engage the drill pipe or disengage the drill pipe from the borehole **402** . Upon user or controller initiated commands,

the device **406** extends until it firmly engages with the inner wall **412** of the borehole **402**.

The anchor mechanism **406** can be disengaged from the borehole **402** upon command. The anchor mechanism may be a hydraulic, pneumatic, or an electro-mechanical device that can be operated or controlled from a surface location or which maybe a fully downhole controlled device. Still referring to **Figure 4A**, a magnetostrictive actuator **404** such as one described above, is preferably mounted within the anchor mechanism **406**. The pipe **410** and the anchor mechanism **406** are coupled in an axially moveable relationship with each other so that the drill pipe **410** can be axially displaced relative to the section **406** along the longitudinal pipe axis **409** when the actuator **404** is activated. The anchor mechanism **406** engages with the borehole **402** to exert sufficient pressure on the borehole wall **412** to ensure that anchor mechanism **406** is not displaced relative to the borehole wall **412** when the actuator **404** is activated. Not shown is a preloading spring as in the other embodiments, however a spring or another preloading device may be used to maintain the magnetostrictive element of the actuator **404** under compression.

The fixed relationship between the anchor mechanism **406** and the borehole **402** creates an acoustic wave "dead end" in the pipe **410** at the anchor mechanism **406**. Anchoring of the pipe **410** causes the mass of the earth to act as the reaction mass. Thus, the dead end at the anchors **406** acts as the reaction mass point and causes the acoustic wave generated by the actuator **404** to travel in the drill pipe along the drill pipe section above the dead end.

Figure 4B is an elevation view of one possible way to configure the embodiment described with respect to **Figure 4A** to achieve a forceful interface with the borehole **402** while allowing axial displacement of the pipe **410**. The pipe **410** includes keeper rings or offsets **418**. Disposed around the pipe **410** and between the offsets **418** are the magnetostrictive material **404**, a free-sliding sleeve or ring **414** and a biasing element or spring **416**. Ribs **406** are mounted on the sleeve **414**, so the ring becomes fixed when the ribs **406** apply force to the borehole wall **412**. When the magnetostrictive material **404** is activated, substantially all of the force is transferred to the offsets **418**, thus axially displacing the pipe **410**. The biasing element **416** ensures a minimum predetermined compression load is maintained on the magnetostrictive material **404**.

Another dead end embodiment according to the present invention is shown in **Figure 4C**. **Figure 4C** shows ribs **406** applying force to the inner wall **412** of the borehole **402**. The ribs **406** are mounted on a lower section of pipe **426** below the actuator **404**. In this embodiment, the upper section of pipe **428** experiences substantially all of the axial displacement when the actuator **404** is excited. Shown in **Figure 4D** is the actuator **404** with a cylindrical magnetostrictive core **420** and coils or windings **422**. The coils **422** are wound around the cylindrical core **420**.

The actuator **404** is attached to offsets **418** located on the upper section of pipe **428** and to the lower section of pipe **426** by any suitable manner, such as with fasteners **424**. A biasing member, (not shown) maintains the actuator **404** in compression to a predetermined amount. The biasing member may be placed above or below the actuator **404**.

The drill pipe **410** may include a section of reduced diameter **430** that is sized to be inserted in the inner bore **436** of the other pipe **428** for added stability between the upper section **428** and lower section **426**. Of course the reduced diameter pipe **430** could also be carried by the upper pipe section **428** and be inserted into the inner bore **436** of the lower pipe **428**. The reduced diameter pipe **430**, which should be rigidly fixed (e.g.

welded or milled as one piece) to the lower section **426**, and have an internal through bore **434** to allow mud to flow for drilling operations. The reduced diameter pipe **430** should have a non-rigid connection such as a steel pin **432** to connect it to the upper sections **428** through a hole or slot in the upper section **428**. This non-rigid connection would provide the necessary horizontal stability and rotational stability while maintaining enough freedom of movement in the vertical (axial) direction for transmitting the data pulses generated by the magnetostrictive element **404**. As described above, either pipe may carry the reduced diameter pipe **430**, and so either pipe may include the rigid or the non-rigid connection.

The configuration just described allows the upper section of pipe **428** to move axially with respect to the lower section of pipe **426**. With the actuator **404** coupled above the ribs **406**, an acoustic wave is transferred mostly through the upper section of pipe **428** to be received at the surface or intermediate location by a receiver **408**. As with all other embodiments described herein, the stiffness of the pipe is decoupled from the actuator **404** movement thereby making transmission more efficient, even at low frequencies.

Figure 5 is an elevation view of a drilling system **500** in a measurement-while-drilling (MWD) arrangement according to the present invention. As would be obvious to one skilled in the art, a completion well system would require reconfiguration; however the basic components would be the same as shown. A conventional derrick **502** supports a drill string **504**, which can be a coiled tube or drill pipe. The drill string **504** carries a bottom hole assembly (BHA) **506** and a drill bit **508** at its distal end for drilling a borehole **510** through earth formations.

Drilling operations include pumping drilling fluid or "mud" from a mud pit **522**, and using a circulation system **524**, circulating the mud through an inner bore of the drill string **504**. The mud exits the drill string **504** at the drill bit **508** and returns to the surface through the annular space between the drill string **504** and inner wall of the borehole **510**. The drilling fluid is designed to provide the hydrostatic pressure that is greater than the formation pressure to avoid blowouts. The mud drives the drilling motor (when used) and it also provides lubrication to various elements of the drill string. Commonly used drilling fluids are either water-based or oil-based fluids. They also contain a variety of additives which provide desired viscosity, lubricating characteristics, heat, anti-corrosion and other performance characteristics.

A sensor **512** and a magnetostrictive acoustic actuator **514** are positioned on the BHA **506**. The sensor **512** may be any sensor suited to obtain a parameter of interest of the formation, the formation fluid, the drilling fluid or any desired combination or of the drilling operations. Characteristics measured to obtain to desired parameter of interest may include pressure, flow rate, resistivity, dielectric, temperature, optical properties tool azimuth, tool inclination, drill bit rotation, weight on bit, etc. The output of the sensor **512** is sent to and received by a downhole control unit (not shown separately), which is typically housed within the BHA **506**. Alternatively, the control unit may be disposed in any location along the drill string **504**. The controller further comprises a power supply (not shown) that may be a battery or mud-driven generator, a processor for processing the signal received from the sensor **512**, a converter for converting the signal to a sinusoidal or pulsed current indicative of the signal received, and a conducting path for transmitting the converted signal to coils of actuator **514**. The actuator **514** may be any of the embodiments as described with respect to **Figures 2-4**, or any other configuration meeting the intent of the present invention.

The acoustic actuator **514** induces an acoustic wave representative of the signal in the drill pipe **504**. A reaction mass **505** may be the lower portion of the drill string **504**, may be a separate mass integrated in the drill string **504**, or may be effectively created with a dead end by using a selectively extendible force application member (see **Figures 2-4**). The acoustic wave travels through the drill pipe **504**, and is received by an acoustic wave receiver **516** disposed at a desired location on the drill string **504**, but which is typically at the surface. A receiver **516** converts the acoustic wave to an output representative of the wave, thus representative of the parameter measured downhole. The converted output is then transmitted to a surface controller **520**, either by wireless communication via an antenna **518** or by any conductor suitable for transmitting the output of the receiver **516**. The surface controller **520** further comprises a processor **522** for processing the output using a program and an output device **524** such as a display unit for real-time monitoring by operating personnel, a printer, or a data storage device.

An embodiment of a production well telemetry system according to the present invention is shown in **Figure 6**. The production well system **600** includes a production pipe **604** disposed in a well **602**. At the surface a conventional wellhead **606** directs the fluids produced through a flow line

608. Control valve **610** and regulator **612** coupled to the flow line **608** are used to control fluid flow to a separator **614**. The separator **614** separates the produced fluid into its component parts of gas **616** and oil **618**. Thus far, the system described is well known in the art.

The embodiment shown for the production well system **600** includes a dead end configuration of an acoustic actuator **624**. A suitable dead end configuration is described above and shown in **Figure 4**. The acoustic actuator **624** includes at least one force application member **622** and a magnetostrictive material **625**. Sensors **620** may be disposed above or below the force application member **622** to obtain desired characteristics and output a signal representing the characteristics. A downhole controller **621** includes a power supply, a processor for processing the output signal of the sensor **620**, a converter for converting the signal to a sinusoidal or pulsed current indicative of the signal received, and a conducting path for transmitting the converted signal to the acoustic actuator **624**. In a production configuration such as shown in **Figure 6**, the controller **621** for the downhole operations may be located on the surface instead of downhole.

Magnetostrictive material **625** in the actuator **624** reacts to the current supplied by the controller by inducing an acoustic wave in the production pipe **604**. The reaction mass is effectively created with a dead end by using a selectively extendible force application member **622** extended to engage the well wall. The acoustic wave travels through the production pipe **604**, and is received by an acoustic wave receiver **626** disposed at any location on the production pipe **604**, but which is typically at the surface in the wellhead **606**. The receiver **626** converts the acoustic wave to an output indicative of the wave, thus indicative of the parameter measured downhole. The output is then transmitted to a surface controller **630** by wireless communication via an antenna **628** or by a conductor suitable for the output of the receiver **626**. The surface controller **630** further comprises a processor for processing the signal using a program and an output device such as a display unit for real-time monitoring by operating personnel, a printer, or a data storage device.

Embodiments of the present invention described above and shown in **Figures 2-6** utilize an acoustic actuator (driver) comprising a magnetostrictive material to generate force within an acoustic transmitter system. Other embodiments to be described below in detail utilize

alternative driver devices to generate forces necessary to resonate a reaction mass.

Figure 7 is a system schematic of an acoustic transmitter having a linear electromagnetic drive according to an alternative embodiment of the present invention. The acoustic transmitter system **700** includes a substantially tubular passageway (tube) **702** having a central bore. The tube **702** may be, for example, a jointed drill pipe, coiled tube or a well production pipe through which pressurized drilling mud, formation fluid or a combination of drilling mud and formation fluid flows. Fluid flow through the tube is a typical environmental condition. However, the present invention is adaptable to tubes having no fluid as well.

An acoustic transmitter assembly **704** is mechanically coupled to the tube **702**. An input device such as an environmental sensor (not shown) is disposed at a predetermined location and is in communication with the acoustic transmitter assembly.

The acoustic transmitter **704** comprises a controller **706**, an electromagnetic drive **708**, a reaction mass **710**, a displacement sensor **712**, and a feedback loop **714**. The controller **706** is in communication with

electromagnetic drive **708** and the feedback loop **712**. The electromagnetic drive **708** is coupled to the reaction mass **710** such that electrical energy communicated from the controller to the electromagnetic drive is transformed into mechanical energy causing linear displacement of the reaction mass **710**. The displacement is in a substantially longitudinal direction with respect to the tube **702**. The displacement sensor **712** is operatively associated with the reaction mass such that displacement of the reaction mass **710** is measured by the displacement sensor **712**. A sensor output signal representative of the measured displacement is communicated to the controller **706** via the feedback loop **714**.

The electromagnetic drive **708** may comprise a first drive **709a** and a second drive **709b** disposed at opposite ends of the reaction mass **710**. One or more biasing elements **716** may be disposed on at least one end of the reaction mass for urging the reaction mass in a longitudinal direction. The biasing element **716** may be a fluid spring such as liquid or gas, metal spring or any other suitable biasing device. Upper and lower plungers **707a** and **707b** are coupled to the reaction mass **710** and extend through the electromagnetic drives **709a** and **709b**.

The controller **706** is preferably a processor-based controller well known in the art. The controller may be disposed within the tube **702** or at a remote location such as at the well surface.

The electromagnetic drive **708** is preferably a linear electromagnetic drive.

The reaction mass **710** is preferably an elongated member extending longitudinally within the passageway. The reaction mass **710** is movably coupled to the tube **702** via the biasing elements **716** when used and electromagnetic drive **708**. In applications without separate biasing elements, the coupling between the reaction mass and electromagnetic drive **708** may be magnetic only.

The displacement sensor **712** may be any device capable of measuring movement of the reaction mass **710**. The sensor **712** preferably measures movement of the reaction mass. The sensor may be an infrared (IR) device, an optical sensor, an induction sensor or other sensor or combination of sensors known in the art.

A sensor output signal is conveyed from the sensor **712** to the controller **706** via the feedback loop **714**. The controller **706** controls electrical power delivery to the electromagnetic drive **708** based in at least part on the output signal of the displacement sensor **712**.

In this configuration, the reaction mass can reciprocally move within the tube at a relatively large resonate amplitude with low frequency. One advantage realized by high amplitude and low frequency is a high signal to noise ratio.

In operation the not-shown environmental sensor sends a first signal indicative of a parameter of interest to the controller **706**. The measured parameter may be any formation, drill string, or fluid characteristic. Examples these characteristics include downhole temperature and pressure, azimuth and inclination of the drill string, and formation geology and formation fluid conditions encountered during the drilling operations.

The first signal is communicated to the controller **706** via a typical conductor such as copper or copper alloy wire, fiber optics, or by infrared transmission. The controller **706** then sends electrical power (energy) to the electromagnetic drive **708** via conductors well known in the art. The

source of electrical power may be selected from known sources suitable for a particular embodiment. The power source may be, for example, a mud turbine, a battery, or a generator.

The controller **706** converts the first signal to a power signal for exciting the electromagnetic drive **708**. The electromagnetic drive then resonates the reaction mass **710** to create an acoustic wave in the structure of the tube **702**. The acoustic wave travels through the tube **702** to a receiver (not shown) capable of sensing the acoustic wave. A converter (not shown) converts the acoustic wave into a second signal representative of the first signal. The second signal may then be converted to a suitable output such as a display on a screen, a printed log or it may be saved via known methods for future analyses.

Figures 8A-8C show various alternative embodiments for a linear electromagnetic drive acoustic transmitter according to the present invention. **Figure 8A** is substantially identical to the system schematic described above and shown in **Figure 7**. **Figure 8A** shows a controller **706** coupled to a tube **702** within the central bore of the tube **702**. All element couplings and operations associated with the embodiment of **Figure 8A** are as described above with respect to **Figure 7**.

Figure 8B shows an alternative electromagnetic drive embodiment wherein a reaction mass **804** includes a central flow path **805** to allow drilling fluid to pass therethrough. Otherwise, the embodiment of **Figure 8B** is substantially identical to the embodiments described above and shown in **Figures 7 and 8A.**

Figures 9A and 9B show alternative embodiments of the present invention having resonant acoustic transmitters. The embodiments described above and shown in **Figures 2-8B** all utilize drive devices that convert electrical energy to force applied to a reaction mass. The embodiments of **Figures 9A** and **9B**, in the alternative, utilize kenetic energy of pressurized drilling fluid flowing in the drillstring to resonate a reaction mass.

Figure 9A shows a portion of drill string **900** comprising a tube **902.** An acoustic transmitter **903** according to an embodiment of the present invention is housed within the tube **902**. The transmitter **903** is a spring-mass system that comprises a reaction mass **904** and a drive device **910**. The reaction mass **904** is slidably disposed within the tube **902**. Guides

906a and **906b** are coupled to the reaction mass **904** to inhibit motion perpendicular to the longitudinal axis of the device.

The transmitter **903** is excited with forces generated through pressure changes in the flow of drilling fluid, which is redirected to the system. The fluid path is altered with a valve **910** or other flow restricting device such that the kinetic energy of the flowing drilling fluid is converted to force applied to the reaction mass **904**.

The drive device **910** is coupled to the reaction mass **904** at preferably one end. The drive device **910** is a fast-operating valve used to restrict fluid flow through the tube thus creating a pressure differential that acts on an area of the reaction mass **904** substantially equal to the bore area of the tube **902**.

The fast operating valve may include a rotating valve or a poppet valve. If a rotating valve is used, the rotating valve could have either axially or radially arranged openings. The rotating valve could be driven by a synchronous motor or a stepper motor to open and close the valve openings using a base frequency and higher or lower frequencies to transmit signals.

A poppet valve is any arrangement of a variable flow restrictor typically comprised of a piston that moves axially and thus closes an orifice partially or completely. A pilot valve (not shown) may be used to reduce the power requirements for a poppet valve, or the high pressure could be used to partially compensate for the forces that have to be created by the valve actuator.

Figure 9B shows an alternative arrangement of an acoustic transmitter **911** using fluid pressure changes to initiate oscillating motion of a reaction mass **912**. Shown is a portion of a drill string **900** similar in most respects to the device shown in **Figure 9A**. The drill string **900** includes a drill pipe **902** having a central bore. An acoustic transmitter **911** according to the present invention is housed within the central bore of the drill pipe **902**.

The acoustic transmitter **911** comprises a reaction mass **912** having a longitudinal bore **914** to allow flow of drilling fluid therethrough. A fast-operating valve **918** is coupled to one end of the reaction mass **912**. The mass is preferably biased with a spring or other suitable biasing element

(not separately shown) to enhance oscillating motion when the valve **918** is operated.

In one arrangement, drilling fluid flows through the central bore **914** with the valve **918** being used to restrict or stop flow altogether at predetermined frequencies.

In another arrangement, an additional channel **916** for fluid flow is located between the outside wall of the reaction mass **912** and the inside wall of the drill pipe **902**. The valve **918** in this arrangement is configured such that no fluid passes through the central bore **914** when the valve is activated. All of the fluid bypasses at the outside of the mass **912** and actuator **918** through the outer channel **916**.

Another embodiment similar to the one just described again has a central bore **914** inner and an outer flow channel **916**. Each path will have a nozzle for constant flow restriction configured such that the flow restriction of the outer channel **916** is substantially equal to the flow restriction in the central bore **914**. This arrangement allows the use of a fluidic valve known in the art as a Coanda valve to direct fluid either to the

outer channel **916** or to the central bore **914** thus creating pulsating forces onto the spring mass combination.

Control of the Coanda valve can be accomplished by either using a control line connecting the two main flow channels of a Coanda at the entrance of these channels or by disturbing the flow at the entrance of one or both main flow channels.

When using a control line, the Coanda valve operates at a stable frequency determined by the dimensions of the control line (length, area of cross-section, shape of cross- section, and fluid properties). In order to switch from the base frequency to another frequency, the dimensions of the cross section are changed. This can be accomplished using, for example, a flow restrictor such as an adjustable valve. Two or more fully or partially parallel control lines may be used to control the frequency by switching between the control lines thus modulating the main frequency.

When using pressure disturbance to control frequency a control line, flow disturbance at the entrance of one or both main flow channels is accomplished, for example by moving an obstacle (not shown) into the flow

path or injecting a small amount of fluid into the entrance of a main channel through a small orifice.

An operational advantage gained by the use of any of the preceding embodiments is that the reaction mass being oscillated by any of these actuators could also be used to apply pulsed forces to the drill bit for the purpose of drilling enhancement. When using the embodiments shown in **Figures 9A-9B** in particular drilling operations would be improved through the pressure pulses and consequently flow pulses helping to clean the bit or the bottom of the hole, and also by changing the hydraulic forces applied to the rock.

Another advantage in using any of these actuators is realized by using the forces generated in the drill pipe as a seismic actuator through the transfer of the forces to the bit.

The actuators described above and shown in **Figures 9A-9B** provide a dual purpose advantage in that they are not only inducing forces into the drill pipe for an acoustic axial signal transmission in the drill pipe but they are also creating pressure pulses traveling to the surface in the

drilling fluid. The drilling fluid pulse provides a redundant signal that may be used to help to improve signal detection at the surface.

Any of the actuators described above can be modified without departing from the scope of the present invention to convert axial forces generated by the reaction mass into a tangential force thus creating a fluctuating torque to the drill pipe. The fluctuating torque may be used as a method of signal transmission that could have less signal attenuation and thus allow transmitting data over a longer distance.

The foregoing description is directed to particular embodiments of the present invention for the purpose of illustration and explanation. It will be apparent, however, to one skilled in the art that many modifications and changes to the embodiment set forth above are possible without departing from the scope and the spirit of the invention. It is intended that the following claims be interpreted to embrace all such modifications and changes.